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Characterization of thin polymer films using terahertz time-domain interferometry

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An interferometer for broadband single-cycle THz pulses is developed based on the Michelson configuration. Total internal reflection of THz pulses in high-resistivity silicon prisms provides a nearly 180° phase shift of one arm relative to the other to achieve destructive interference. We show that due to automatic compensation for laser fluctuations by the interferometer, it is possible to measure the index and absorption of thin-film samples with more accuracy than is achievable with standard THz time-domain spectroscopy. We demonstrate characterization of the complex index of refraction of 2 μ m thick Mylar (polyester) films. By measuring the signal amplitude directly in the time domain, the interferometer can be used for rapid measurements of film thickness with a resolution of better than 1 μ m. © 2001 American Institute of Physics. [DOI: 10.1063/1.1389823]

The measurement of thin films¹ is one of the enabling roles of optics in modern day industry.² Accurate measurement and control of film thickness are critical to applications from semiconductor processing to food packaging. However, well developed optical techniques such as variable angle spectroscopic ellipsometry and phase-contrast microscopy are not applicable for measurement of opaque films.

The recently developed techniques of THz time-domain spectroscopy (THz TDS)¹ and THz tomography^{3,4} have been shown to be capable of performing measurements on, and images of, samples which are opaque in the visible and near-infrared regions of the spectrum. The utility of THz TDS is limited in the case in which the sample is very thin, or has a low index and absorption, since it is very difficult to distinguish changes in the THz pulse caused by the sample from those caused by long term fluctuations in the driving laser source or experiment. Using standard THz TDS, 172 μ m films of polyimide have been characterized.⁵ In transmission measurements, rapid sample dithering has permitted differential measurements of parylene-N films.⁶ An interferometer incorporating the Gouy phase shift has permitted reflection measurements of voids in Teflon as small as 12.5 μ m.⁷

The experimental setup consists of a Michelson type interferometer configuration inserted into a standard THz TDS system as shown in Fig. 1. The THz source is a coplanar transmission line biased at 40 $V_{\rm dc}$ which generates freely propagating pulses of THz electromagnetic radiation. The radiation emitted covers a 0.3–1.5 THz bandwidth [see the reference spectrum in Fig. 3(b)] and is collected by a silicon lens and collimated by a parabolic mirror. The THz beam (shown by thick lines) is split by a 0.35 mm thick silicon beam splitter into reference and sample pulse trains. The two THz pulse trains are incident on silicon right angle prisms which act as roof reflectors. One face of the sample arm prism is coated with a 60 nm thick layer of aluminum deposited by thermal evaporation. After passing through the prisms, the separate THz pulses are again made coincident

In THz TDS, a sample with complex refractive index, $n(\omega) = n_r(\omega) - i n_i(\omega)$, is placed in the THz beam and the electric field $E_{\rm samp}(t)$ transmitted through, or reflected from, the sample is measured. The sample is then removed, and a second reference scan is measured, $E_{\rm ref}(t)$. The numerical Fourier transform of the time dependent data yields the complex amplitude spectra $E_{\rm samp}(\omega)$ and $E_{\rm ref}(\omega)$. The ratio of the sample spectrum to the reference spectrum determines the phase and amplitude shift of the THz pulse interacting with the sample. Assuming a transmitted pulse going through a sample of thickness d

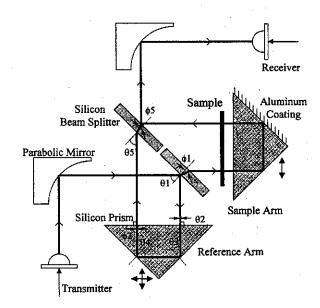


FIG. 1. Diagram of the THz interferometer. The beam splitters are independently adjustable and the prisms can be translated into the directions indicated by the arrows. The incidence angle on the prism faces $(\theta_2$ and $\phi_2)$ is 0° .

by the second beam splitter. A second parabolic mirror collimates the superposition of the two THz pulse trains which are then incident on the 50 μ m receiver antenna. Thin-film samples are placed in the sample arm in the position shown in Fig. 1.

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$$\frac{E_{\text{samp}}(\omega)}{E_{\text{ref}}(\omega)} = \exp\{-ik_0[n_r(\omega) - 1 - in_i(\omega)]d\},\tag{1}$$

with $k_0 = \omega/c$. With the power absorption coefficient given by $\alpha = 2\omega n_i(\omega)/c$, both the real part of the refractive index and the absorption spectra are determined from the ratio of the measurements. For samples with high index the Fresnel transmission coefficients, $t_{12}(\omega)$ and $t_{21}(\omega)$, on the input and output faces, respectively, must be included. ¹⁰

In the THz TDS system shown in Fig. 1, the THz pulse is split into both sample, $E_{\text{samp}}(t)$, and reference, $E_{\text{ref}}(t)$, pulses and a single measurement returns the superposition $E(t) = E_{\text{samp}}(t) + E_{\text{ref}}(t)$. The measured fields from each arm are then given by the incident field multiplied by the Fresnel coefficients along the beam path. The Fresnel coefficients 11 are defined as r_{12}^{θ} for reflection and t_{12}^{θ} for transmission where the subscript "12" corresponds to an air-silicon interface and "21" to a silicon-air interface at incident angle θ . The Fresnel coefficient $r_{2M}^{\theta 4}$ is the reflection coefficient at the silicon-metal interface. By rotating the prisms to minimize the time delay, the interferometer is aligned so $\theta_3 = 45^{\circ}$ and $\theta_2 = \theta_4 = 0^{\circ}$ and for this optimal alignment $\theta_1 = \theta_5 = 45^{\circ}$. Contrary to intuition, the silicon-metal reflection, $r_{2M}^{\theta 4}$, has a value of +1 when the field is polarized in the plane of incidence (P). 11 The complex coefficient $r_{21}^{45^{\circ}} = -0.983 + 0.186i$ corresponds to total internal reflection with $|r_{21}^{45}|=1$ with a phase angle of 169.7°. The sample transmission function, $T_s(\omega)$ is given by

$$T_s(\omega) = t_{1S}t_{S1} \exp\{-ik_0[n_r(\omega) - 1 - in_i(\omega)]d\},$$
 (2)

where t_{1S} and t_{S1} are the Fresnel coefficients for $\theta=0^{\circ}$ and we assume the sample index is small so secondary reflections can be ignored.

With the reference arm phase defined to be 0° and $T_s(\omega) = 1$, $E_{\text{ref}}(\omega) = 0.24E_0(\omega)$ and $E_{\text{samp}}(\omega) = -0.24E_0(\omega)T_s(\omega)\exp(i10.3^{\circ})$. This phase shift arises from the frequency independent Fresnel reflection coefficient which has complex value for total internal reflection. The temporal phase shift has been observed previously with THz pulses. ¹² Due to this phase shift between the arms, even under optimal alignment conditions complete destructive interference of the THz wave forms is impossible to achieve. A numerical analysis for this system shows that the best extinction possible in the time domain is approximately 2.5% of the signal propagated by one arm.

The measured pulses in the reference arm, $E_{\rm ref}(t)$, and sample arm, $E_{\rm samp}(t)$, obtained by blocking one arm and measuring the signal in the other arm are shown in Fig. 2(a). The measured signal (points) in the sample arm is also shown when a 2 μ m thick Mylar[®] sample is placed in this arm. The small value of $k_0(n-1)d$ makes these two THz pulses nearly indistinguishable. Figure 2(b) shows the measured interferometer signal with both the sample and reference arms open. The measured peak to peak signal here is 3.5% of the difference between the peaks of the reference and sample arms measured individually. The slight additional signal over the 2.5% calculated minimum is attributed to slight misalignments of the THz beam. The signal measured with both arms open and a nominally 2μ m Mylar film as a sample, $E_{\rm meas}(t)$, is shown in Fig. 2(b).

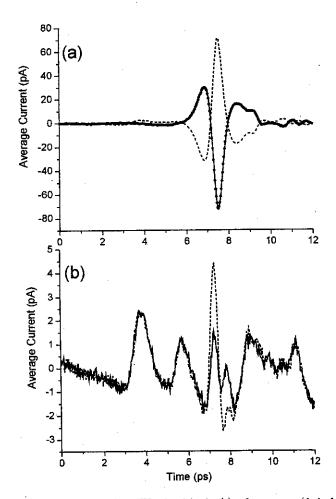


FIG. 2. Measurement of the THz signal in the (a) reference arm (dashed line) and sample arm (solid line). The dotted line represents the sample arm when the sample is placed in the arm. (b) The measured signal with no sample in the beam $E_{\Phi}(t)$ is shown as a solid line and the signal, $E_{\rm meas}(t)$, with a 2 μ m thick Mylar film (dashed line).

For the interferometer, the measured frequency dependent signal, $E_{\rm ref}(\omega) + E_{\rm samp}(\omega)$ can be written as

$$E_{\text{meas}}(\omega) = E_{\text{ref}}(\omega) \{ 1 - \exp(-ik_0[n(\omega) - 1]d + i\Phi(\omega)) \},$$
(3)

where we have assumed the index and absorption of the sample are small so that $t_{1S} \cong t_{S1} \cong 1.6$ The phase term, $\Phi(\omega)$, accounts for both the 10.3° phase difference as well as a frequency dependent term accounting for small misalignments of the sample arm. $\Phi(\omega)$ is determined by taking a scan with no sample in the interferometer, $E_{\Phi}(\omega) = E_{\text{ref}}(\omega) \times (1 - e^{i\Phi(\omega)})$. Measurements of the reference arm pulse, $E_{\text{ref}}(\omega)$, and the interferometer signal with, $E_{\text{meas}}(\omega)$, and without, $E_{\Phi}(\omega)$, a sample permit determination of the complex refractive index:

$$n_r(\omega) - in_i(\omega) = \frac{-i}{k_0 d} \ln \left(\frac{E_{\text{meas}}(\omega) - E_{\Phi}(\omega)}{E_{\Phi}(\omega) - E_{\text{ref}}(\omega)} + 1 \right) + 1.$$
(4)

For thin samples of low index, $k_0[n(\omega)-1]d \le 1$ which permits expanding the exponential in Eq. (3) as a series, $\exp(x) \cong 1+x$. The complex index can then be calculated by dividing the measured signal by the reference when the phase shift, $\Phi(\omega)$, is known:

$$\frac{E_{\text{meas}}(\omega)}{E_{\text{ref}}(\omega)} \cong k_0 n_i(\omega) d + i k_0 [n_r(\omega) - 1] d + i \Phi(\omega). \tag{5}$$

THz interferometry is capable of determining small changes in the film thickness-index product directly from the time-domain data without measurement of the full THz pulse. The effect of a film of index, $n = n_0 + \Delta n(\omega)$ with $\Delta n(\omega) \ll n_0$ and $\alpha L \ll 1$, and thickness, d, is to shift the THz pulse in time by an amount $\Delta t = d(n-1)/c$ for a single pass of the THz pulse through the film and $\Delta t = 2d(n-1)/c$ for a double pass. In this case, with no sample in the beam, the measured electric field in the reference arm given by $E_{ref}(t)$ and that of the sample arm $E_{\text{samp}}(t) = -E_{\text{ref}}(t) + E_{\Phi}(t)$, where $E_{\Phi}(t)$ is the small residual time signal due to the phase shift, $\Phi(\omega)$. Inserting the sample shifts the pulse in the sample arm by an amount Δt . With the time shift, the measured signal is $E_{\text{meas}}(t) \cong E_{\text{ref}}(t) - E_{\text{ref}}(t - \Delta t) + E_{\Phi}(t)$. With the known $E_{\Phi}(t)$ subtracted from the data, the time shifted reference pulse can be expanded in a Taylor series with only the first order terms being retained for small Δt . In this case

$$E_{\text{meas}}(t) = E_{\text{ref}}(t) - E_{\text{ref}}(t - \Delta t) \cong \Delta t E'_{\text{ref}}(t), \tag{6}$$

where the prime corresponds to the time derivative. The quantity $\Delta t = d(n-1)/c$ can be determined by numerically integrating $E_{\rm meas}(t)$ and determining Δt by a comparison to the known reference pulse. The film thickness-index product given through Δt is directly proportional to the size of the measured signal, $E_{\rm meas}(t)$, from the THz interferometer.

To demonstrate the measurement sensitivity of the interferometer we measure free standing films of nominally 2 μ m thick films of DuPont type C Mylar® polyester film. 13 The film, stretched taut to eliminate wrinkles, was mounted on a frame placed in the sample arm of the interferometer. The film thickness, independently measured at several points on the sample. Measurements of the refractive index-thickness product of the Mylar film extracted directly from the timedomain data utilizing Eq. (6) are given in Fig. 3(a) from the data shown in Fig. 2. With both arms open and no sample in the beam, the solid line is $E_{\Phi}(t)$, due to the frequency independent phase shift and small misalignments. To find the film thickness, $E_{\Phi}(t)$ is subtracted from the measured data of Fig. 2(b), then integrated, and a value of Δt is found which, when multiplied by the integrated data, will return the reference pulse shape. The reference pulse is shown as a solid line in Fig. 3(a) with the fit (data points) of the Mylar films using a value of Δt of 10.5 fs, corresponding to $2d(n_r-1)$ of 3.15 μ m. Using the published 1 GHz dielectric constant of $(n_r)^2 = \varepsilon_r = 2.8$, ¹³ this returns a value of $d = 2.3 \,\mu\text{m}$ which agrees well with the measured film thickness.

The frequency dependent index and absorption, determined from Eq. (5), are shown in Fig. 3(b). The absorption of this thin film is not measurable since the absorption length $2\alpha L \ll 1$. The index of refraction is close to that of the published dc dielectric constant. The oscillations in the data are in part due to water vapor in the beam path. These results are in good agreement with the estimated index and film thickness obtained directly in the time domain from Fig. 3(a).

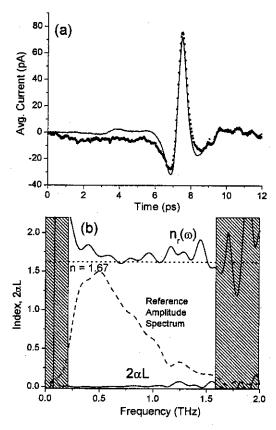


FIG. 3. (a) Measured reference pulse (solid line) $E_{\rm ref}(t)$ and the fit of the measured pulse with background phase subtracted following Eq. (6) with Δt of 10.5 fs. (b) Measured real refractive index (upper solid line) and absorption×length (lower solid line) determined using Eq. (5). The dotted line is the 1.67 index of Mylar at 1 GHz while the dashed curve is the reference pulse spectral amplitude.

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